

Analysis of High Average Breakdown Fields between Gate and Drain in AlGaIn/GaN HEMTs with High- k Passivation Layer

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ABSTRACT

We make a two-dimensional analysis of breakdown characteristics of AlGaIn/GaN HEMTs with a high- k passivation layer, where a deep acceptor above the midgap is considered in a buffer layer. It is shown that the breakdown voltage V_{br} becomes higher when the relative permittivity of the passivation layer ϵ_r is higher. In the case where the deep-acceptor density is relatively high, V_{br} is determined by impact ionization of carriers, and it reaches about 500 V at the gate-to-drain distance L_{GD} of 1.5 μm when ϵ_r is 60. This corresponds to an average electric field of about 3.3 MV/cm which is nearly equal to the theoretical limit of GaN. When ϵ_r is higher than 30, V_{br} becomes higher when L_{GD} becomes longer, and it becomes about 930V and 1360 V when $L_{GD} = 3 \mu\text{m}$ and 5 μm , respectively at $\epsilon_r = 60$. These voltages correspond to average electric fields of about 3 MV/cm and 2.7 MV/cm between the gate and the drain, respectively.

Keywords: GaN HEMT, breakdown voltage, buffer layer, deep acceptor, high- k passivation layer

1 INTRODUCTION

AlGaIn/GaN HEMTs are now receiving great interest for application to high-power microwave devices and high power switching devices [1, 2]. To improve the power performance and the breakdown voltage of FETs, the introduction of field plate is shown to be effective [3-8], but it may increase the parasitic capacitance, leading to degrading the high-frequency performance. The average electric field at breakdown between the gate and the drain is usually about 1 MV/cm. In a previous work [9, 10], as another method to improve the breakdown voltage of AlGaIn/GaN HEMTs, we proposed a structure including a high- k passivation layer, and showed that the breakdown voltage increased significantly. We assumed an undoped semi-insulating buffer layer where a deep donor compensates a deep acceptor. Recently, Fe- and C-doped semi-insulating buffer layers are often adopted and they acts as deep acceptors [11-15]. Therefore, in this work, we analyze AlGaIn/GaN HEMTs with a buffer layer including only a deep acceptor, and studied how the breakdown voltage is influenced by its density and the gate-to-drain distance.

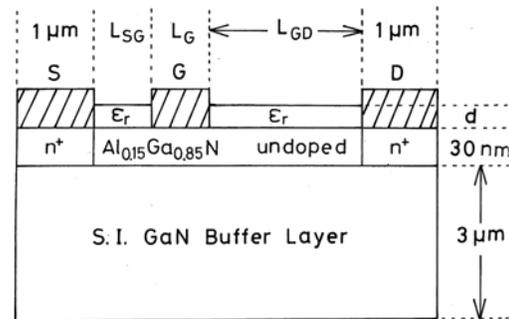


Figure 1: Device structure analyzed in this study

2 PHYSICAL MODEL

A device structure analyzed here is shown in Fig.1. The gate length is 0.3 μm and the gate-to-drain distance L_{GD} is varied between 1.5 μm and 5 μm . The passivation layer's thickness is 0.1 μm . We vary the relative permittivity of the passivation layer ϵ_r as a parameter. Here, we adopt a Fe-doped semi-insulating buffer layer, where the Fe-related level (E_{DA}) is set to 0.5 eV below the bottom of conduction band [11, 15]. The Fe-related level is a deep acceptor. The deep acceptors act as electron traps. The deep-acceptor density N_{DA} is set to 10^{17} cm^{-3} and $2 \times 10^{17} \text{ cm}^{-3}$ [16, 17]. Basic equations to be solved are Poisson's equation having the ionized deep-acceptor density term and electron and hole continuity equations which include a carrier loss rate via the deep acceptor and an impact ionization rate [10, 18-20] and these are solved numerically.

3 DEPENDENCE ON DEEP-ACCEPTOR DENSITY

Figs.2 and 3 shows calculated off-state drain current (I_D) – drain voltage (V_D) curves as a parameter of the relative permittivity of passivation layer ϵ_r , where N_{DA} is 10^{17} and $2 \times 10^{17} \text{ cm}^{-3}$, respectively. Here, $L_{GD} = 1.5 \mu\text{m}$. In both cases, when ϵ_r is low (≤ 10), a sudden increase in drain current due to impact ionization determines the breakdown voltage V_{br} . In this region, the drain current becomes equal to the gate current. In the case of $N_{DA} = 10^{17} \text{ cm}^{-3}$, when ϵ_r becomes high (≥ 30), I_D reach a critical value (1 mA/mm) before a sudden increase in I_D . In this case the drain current is much higher than the gate current, and hence the buffer

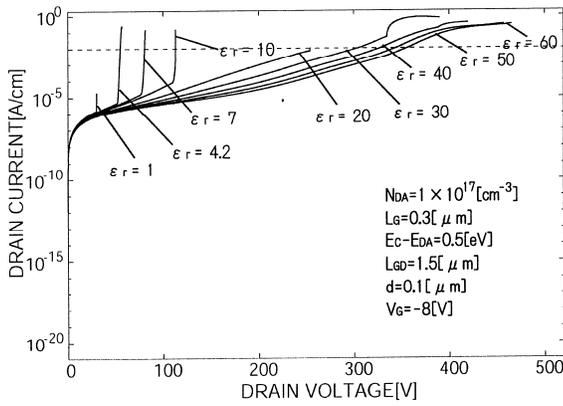


Figure 2: Calculated off-state (a) $I_D - V_D$ curves and (b) $I_G - V_D$ curves when $N_{DA} = 10^{17} \text{ cm}^{-3}$. The dotted lines indicate 1 mA/mm.

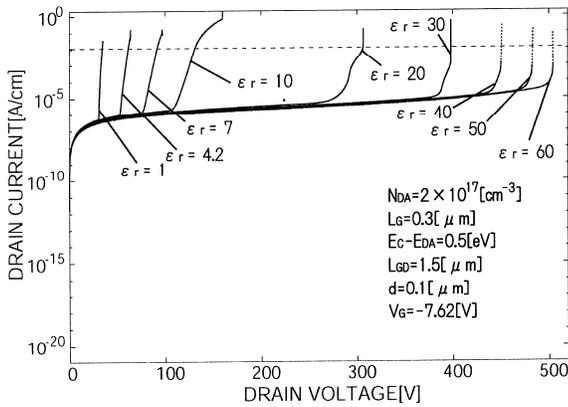


Figure 3: Calculated off-state (a) $I_D - V_D$ curves and (b) $I_G - V_D$ curves when $N_{DA} = 2 \times 10^{17} \text{ cm}^{-3}$. The dotted lines indicate 1 mA/mm.

leakage current determines V_{br} . Note that V_{br} is defined here as the drain voltage when I_D becomes 1 mA/mm. In Figs.2 and 3, V_{br} increases as ϵ_r increases. This is because the electric field at the drain edge of the gate is reduced when ϵ_r becomes high. In the case of $N_{DA} = 2 \times 10^{17} \text{ cm}^{-3}$, even if ϵ_r becomes high (≥ 30), I_D increase suddenly due to impact ionization of carriers and I_D is nearly equal to I_G in this region, and the breakdown voltages are higher than those for $N_{DA} = 10^{17} \text{ cm}^{-3}$. This is because the buffer leakage current is reduced for $N_{DA} = 2 \times 10^{17} \text{ cm}^{-3}$ due to a steeper barrier at the channel-buffer interface [21]. In the case of ϵ_r is 60, V_{br} reaches about 500 V, which corresponding to an average electric field of about 3.3 MV/cm between the gate and the drain. This value is nearly equal to the theoretical limit of GaN. Fig.4 shows electric field profiles at the heterojunction interface for the case of $N_{DA} = 2 \times 10^{17} \text{ cm}^{-3}$. Here, ϵ_r is 60. The electric field profiles are almost uniform at $V_D = 504 \text{ V}$.

4 DEPENDENCE ON GATE-TO-DRAIN DISTANCE

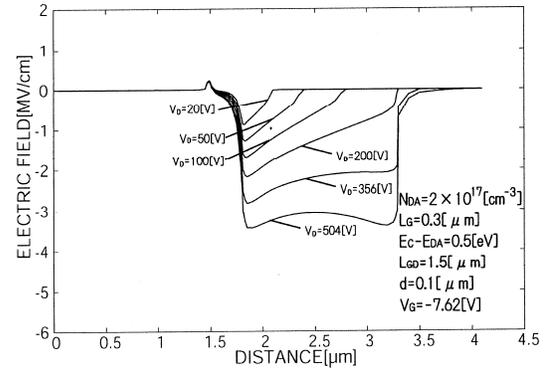


Figure 4: Electric field profiles along the heterojunction interface. $\epsilon_r = 60$. $N_{DA} = 2 \times 10^{17} \text{ cm}^{-3}$. $L_{GD} = 1.5 \mu\text{m}$.

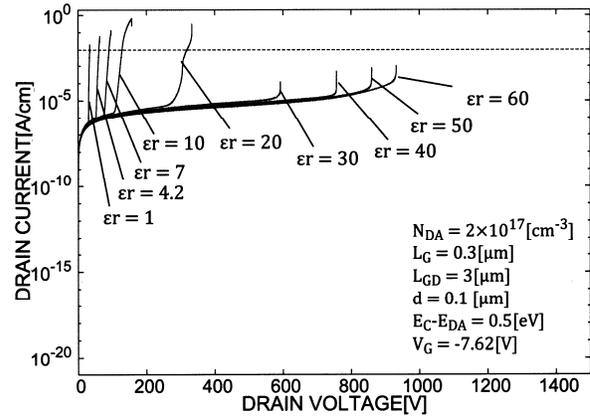


Figure 5: Calculated off-state $I_D - V_D$ curves of AlGaIn/GaN HEMTs when $L_{GD} = 3 \mu\text{m}$. $N_{DA} = 2 \times 10^{17} \text{ cm}^{-3}$.

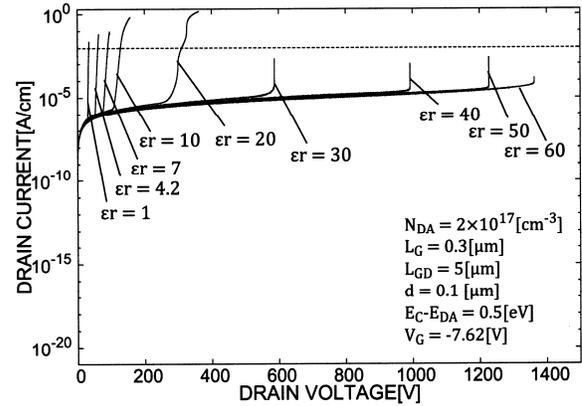


Figure 6: Calculated off-state $I_D - V_D$ curves of AlGaIn/GaN HEMTs when $L_{GD} = 5 \mu\text{m}$. $N_{DA} = 2 \times 10^{17} \text{ cm}^{-3}$.

Figs.5 and 6 show calculated off-state $I_D - V_D$ curves as a parameter of ϵ_r , where the gate-to-drain distance L_{GD} is 3 μm and 5 μm , respectively. Here, $N_{DA} = 2 \times 10^{17} \text{ cm}^{-3}$. In both cases, I_D increases suddenly due to impact ionization of carriers because in the region where I_D increases suddenly, I_D is nearly equal to the gate current I_G (not shown here), as is similar to the case shown in Fig.3. When

ϵ_r is high, the onset voltage for current rise becomes higher in the case of longer L_{GD} (5 μm). Although in some cases, I_D does not reach 1 mA/mm due to the convergence problem, we regard this onset voltage as the breakdown voltage. Fig.7 shows the breakdown voltage V_{br} as a function of ϵ_r , with L_{GD} as a parameter. It is seen that when ϵ_r becomes higher than 30, V_{br} becomes higher when L_{GD} becomes longer. In the case of $\epsilon_r = 60$, V_{br} becomes about 930 V and 1350 V, respectively when L_{GD} is 3 μm and 5 μm . These voltages correspond to average electric fields of about 3.1 MV/cm and 2.7 MV/cm between the gate and the drain, respectively. These values are close to the theoretical limit of GaN (~ 3.3 MV/cm). These suggest that the electric field profiles may be rather uniform between the gate and the drain in these cases

Fig.8 shows a comparison of electric field profiles at the heterojunction interface between the two cases with (a) $L_{GD} = 3$ μm and (b) $L_{GD} = 5$ μm . Here, ϵ_r is 60. When $L_{GD} = 3$ μm , the high electric field region reaches the drain at $V_D = 420$ V, as seen in Fig.8(a). On the other hand, when $L_{GD} = 5$ μm , it reaches the drain at $V_D = 800$ V, as seen in Fig.8(b). At this voltage, when $L_{GD} = 3$ μm , the electric fields at the drain side become very high (~ 3 MV/cm), and the electric field at the drain edge of the gate becomes higher than 3 MV/cm. Then, at $V_D = 932$ V which is the breakdown voltage, the electric field at the drain edge of the gate reaches the critical electric field, resulting in breakdown. On the other hand, when $L_{GD} = 5$ μm , the electric field at the drain edge of the gate is around 3 MV/cm at $V_D = 800$ V. Then, the electric fields between the gate and the drain increase, leading to the breakdown at $V_D = 1362$ V where the electric field at the drain edge of the gate reaches the critical electric field. Therefore, the breakdown voltage becomes higher for longer L_{GD} . It is also seen that at the breakdown, electric field profiles between the gate and the drain are rather uniform in both cases.

5 CONCLUSION

A two-dimensional analysis of breakdown characteristics of AlGaIn/GaN HEMTs with a high- k passivation layer has been performed, where a deep acceptor above the midgap is considered in the buffer layer. It has been ascertained that the breakdown voltage V_{br} becomes higher when the relative permittivity of the passivation layer ϵ_r is higher. In the case where the deep-acceptor density is relatively high, V_{br} is determined by impact ionization of carriers, and it reaches about 500 V at the gate-to-drain distance L_{GD} of 1.5 μm when ϵ_r is 60. This corresponds to an average electric field of about 3.3 MV/cm between the gate and the drain. This value is nearly equal to the theoretical limit of GaN. It has also been shown that when ϵ_r is higher than 30, V_{br} becomes higher when L_{GD} becomes longer, and it becomes about 932 V and 1362 V when $L_{GD} = 3$ μm and 5 μm , respectively at $\epsilon_r = 60$. These values correspond to average electric fields of about

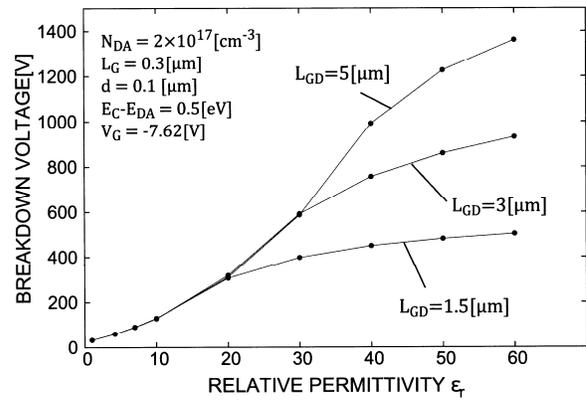


Figure 7: Breakdown voltage V_{br} versus ϵ_r curves as a parameter of L_{GD} . $N_{DA} = 2 \times 10^{17} \text{ cm}^{-3}$.

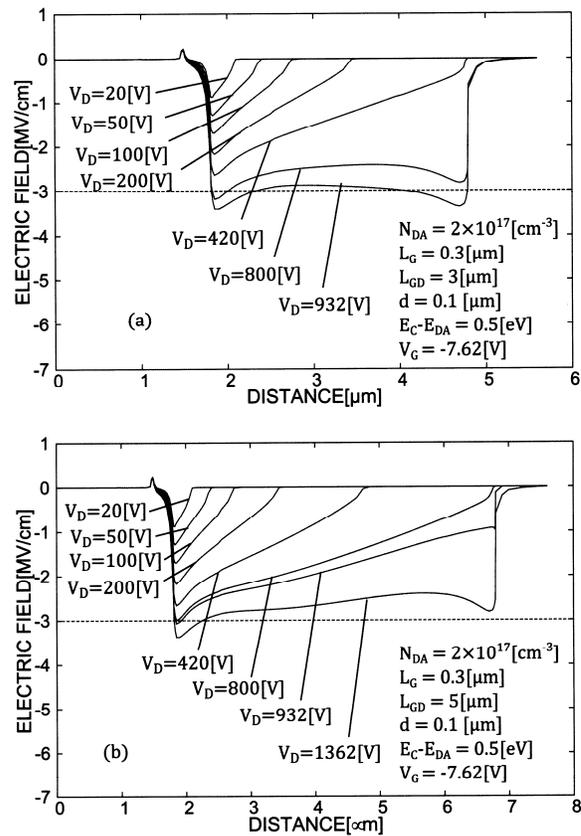


Figure 8: Electric field profiles along the heterojunction interface.. $N_{DA} = 2 \times 10^{17} \text{ cm}^{-3}$ and $\epsilon_r = 60$. (a) $L_{GD} = 3$ μm , (b) $L_{GD} = 5$ μm .

3 MV/cm and 2.7 MV/cm between the gate and the drain, respectively.

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