

High flux nanocomposite hollow fiber membrane for hemodialysis

Surendra Kumar Verma¹, Akshay Modi¹, Atul Kumar Singh², Rohit Teotia³ and Jayesh Bellare^{1,2,4*}

¹Department of Chemical Engineering, ²Centre for Research in Nanotechnology & Science,

³Department of Biosciences and Bioengineering, and ⁴Wadhwani Research Center for Bioengineering,

Indian Institute of Technology Bombay, Mumbai-400076, India

*Corresponding author: jb@iitb.ac.in, Phone: +919820605364

ABSTRACT

Nanocomposite zeolite based hollow fiber membranes (HFM) were synthesized using polyethersulfone (P) as a base polymer, vitamin E TPGS (T) as an additive, and nano-zeolite (NZ) as a filler. Such membranes would have widespread applications, but one goal was to improve outcomes in hemodialysis for kidney failure patients. The resulting nanocomposite membranes materials (called PT-NZ) were spun based on dry-wet spinning method based on phase inversion. The additive and filler helped nodular organization of the polymer into nano-sized domains with numerous pores inbetween, and improved transport properties. They also helped with presenting a more biocompatible surface to the blood and thereby improved hemocompatibility. The PT-NZ membranes were used to fabricate modules consisting of bundles of fibers, and the modules were, in turn, fabricated into mini dialysers. The ultrafiltration coefficient of such PT-NZ HFM-based module (of about 274 mL/m²-hr-mm of Hg) was about 1.5-times higher than that of the commercial (F60S) membrane (about 152 mL/m²-hr-mm of Hg). The bovine serum albumin BSA rejection in aqueous mixtures was found 93.98 %. The toxin clearance performance of lab-scale PT-NZ HFM-based hemodialyzer with uremic toxin spiked goat blood was remarkably higher (about 5X more reduction ratio) than that of commercial F60S hollow fibers. Hence, the synthesized PT-NZ HFM can be a potential membrane material for the hemodialysis application. The newly made HFM reported here could help in decreasing the total treatment time and reducing side-reactions during dialysis for those end stage kidney disease (ESRD) patients dependent on hemodialysis.

Keywords: Nanocomposite hollow fiber membrane; hemocompatibility; ultrafiltration coefficient; solute rejection; uremic toxin clearance

1 INTRODUCTION

Chronic kidney disease (CKD) is one of the major diseases that the World population is facing today. Lakhs of people die annually due to lack of affordable treatment available. In addition to this, there is a tremendous shortage of donor organs compared to the required ones. So, dialysis is the most promising alternative solution to these patients.

Hemodialysis is widely preferred dialysis technique because it employs an extracorporeal device resulting in minimal side-reactions [1]. Hemodialysis requires a blood purification device which is a hollow fiber membrane (HFM)-based dialyzer. The unit removes the uremic toxins from the blood coming out from the CKD patient body and circulates the purified blood back to the patient body [2].

Currently, polyethersulfone (PES) and polysulfone are the two most widely used polymers for fabrication of HFM for hemodialysis [3, 4]. Efforts are underway to improve the separation performance of these HFM. In addition to this, biocompatibility also needs to be improved to avoid any side-reactions. In this context, additives, e.g., d-glucose monohydrate, polyethylene glycol, polyvinylpyrrolidone and monosodium glutamate have been used [5-9].

In this study, novel HFM were manufactured via dry-wet spinning technique using PES (or P) as base polymer, Vitamin E D- α -Tocopherol polyethylene glycol succinate (Vit. E TPGS or T) as an additive and nanozeolite (NZ or N) as a filler. The prepared HFM were characterized and evaluated for hemocompatibility using human blood. Permeability studies were also performed which included ultrafiltration coefficient and bovine serum albumin (BSA) solute rejection of the HFM. Finally, these HFM were used to make lab-scale prototypes of hemodialyzers to test for uremic toxin clearance performance using toxin spiked goat blood. The performance-comparison was also made with the commercial (F60S) HFM.

2 MATERIALS AND METHODS

2.1 Materials

PES (Ultrason E 6020 P), Vit. E TPGS (NF grade) and N-Methyl-2-pyrrolidone (NMP) were procured from BASF (Germany), Isochem (France), and Spectrochem (India), respectively. NZ (LucidotNZ 40) (particle size 40–60 nm) was purchased from M/s. Clariant Produkte (Germany). All the chemicals and reagents were commercially procured either from Merck (Germany) or Sigma Aldrich (USA), and were used without any purification. Urea and creatinine (extrapure) were bought from SD Fine-Chem (India). Commercial dialyzer (F60S) was procured from Fresenius Medical Care (USA).

2.2 Fabrication of HFM

Polymer dope solution of specified composition was prepared to fabricate HFM using indigenous pilot plant using dry-wet spinning method based on liquid-liquid phase separation [10]. The process parameters were listed in Table 1.

Table 1: Process parameters for HFM manufacturing

Temperature (°C)	25		
R.H. (%)	50-60		
Dope comp. (% w/w)	Samples	PES	TPGS
	PT	18	10
	PTN-25	18	10
	PTN-50	18	10
	PTN-75	18	10
Bore comp.	DI water + 33% (v/v) NMP		
Dope/bore temperature (°C)	25		
Dope/bore flow rate (ml/min)	2		
Air gap (cm)	45		
Coagulation/rinse bath composition	DI water		
Coagulation bath temperature (°C)	45		

2.3 HFM Characterization

Surface morphology of HFM was studied using scanning electron microscopy (SEM) (JEOL JSM-7600F, Japan).

2.4 Fabrication of Lab-scale HFM-based Hemodialyzer

Lab-scale modules of PT, PTN-25, PTN-50, PTN-75 and F60S HFM were made by potting HFM ends with Araldite® and sealing fibers in the Teflon™ tube. These modules were used in ultrafiltration coefficient and BSA solute rejection. Next, these modules were then housed in an acrylic pipe to make lab-scale HFM-based hemodialyzers, and the two ends were then sealed using Araldite®. The exposed surface area was kept constant in all dialyzers. The prepared hemodialyzers were used for the uremic toxin clearance study with toxin spiked goat blood. The representative picture of the lab-scale hemodialyzer is shown in Figure 1.



Figure 1: The representative pictures of lab-scale HFM-based hemodialyzer.

2.5 Hemocompatibility studies of HFM

The prepared HFM were studied for the hemocompatibility (hemolysis and platelet adhesion) as per the protocols followed in our previous study [11]. The blood was taken from a healthy donor as per the prescribed institute norms. Also, HFM samples were equilibrated with NSS.

Hemolysis: The hematocrit obtained from the centrifuged human blood was incubated with HFM samples for 1 h at 37 °C and 5 % CO₂ in incubator (Thermo Scientific™). DI water and NSS were used as positive and negative controls, respectively. Then, the samples were centrifuged at 1000x g for 5 min. RBC lysis was quantified to calculate hemolysis ratio (HR).

Platelet adhesion: The supernatant having PRP obtained from the centrifuged human blood was collected and was incubated with HFM samples for 2 h at 37 °C and 5% CO₂ in incubator. The samples were gently washed with NSS, and fixed with 3% glutaraldehyde. Then, the samples were dried with ethanol-water solutions. The samples were coated with Au/Pd using sputter coater (JEOL JFC-1600, Japan), and the cell attachment and activation on different HFM samples were observed under SEM.

2.6 Separation Performance

The ultrafiltration coefficient and BSA solute rejection were measured following the protocols and equations mentioned in our previous study [12]. The cross flow filtration system was used for the studies.

Ultrafiltration coefficient: DI water was pumped at a constant flow rate of 60 ml/min through the lumen of the HFM-based module for 2 h, with the collection of permeate at a regular interval of 15 min., maintaining the pressure difference across the membrane module as 50 kPa.

BSA solute rejection: BSA stock solution (1 g/l) was pumped at a constant value of flow rate (60 ml/min) through the lumen of HFM-based module for 30 min., keeping the transmembrane pressure 50 kPa. After 30 min., permeate was collected and the amount of BSA was determined using BSA analysis kit (Micro BCA Protein Assay Kit, Pierce Biotechnology, IL, United States).

Toxin clearance study with toxin-spiked goat blood: The goat blood was collected as per the standard protocol, and the values of urea, creatinine and phosphate in goat blood were spiked upto the respective levels in CKD stage-5 patients, or popularly known as end-stage renal disease

(ESRD) patients. Dialysis procedure and the dialysis circuit were the same as mentioned in the section “Hemodialysis using a simulated solution” of IS/ISO 8637:2004. Pre-and post-dialysis blood samples were collected and sent to an ISO 9001:2008 certified pathology laboratory for the biochemistry tests to determine the values of toxins (urea, creatinine and phosphate).

3 RESULTS AND DISCUSSION

3.1 HFM Characterization

Figure 2 shows the SEM images of the different asymmetric HFM samples (PT, PTN-25, PTN-50 and PTN-75) prepared in this study. The finger-like structures in the skin layer of the HFMs and the presence of micro to macro voids in the layer towards support layer are also visible. HFMs are predominantly porous.

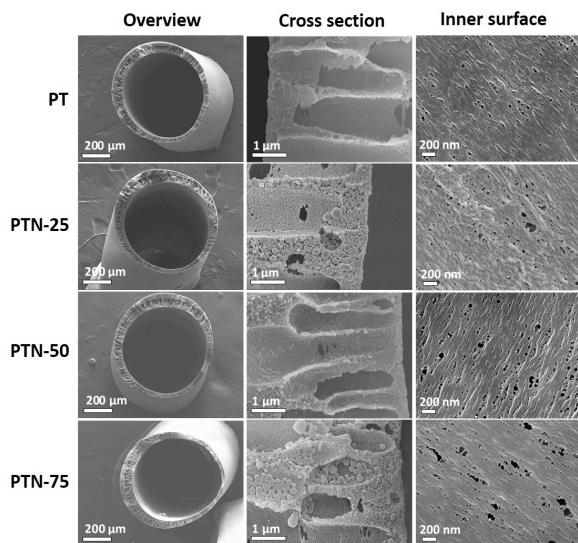


Figure 2: SEM micrographs of the prepared HFMs. Assymmetric HFMs showing more porous structures.

3.2 Hemocompatibility studies of HFMs

Hemolysis: Sheer-force generates due to the flow of blood, which may lead to the rupturing of red blood cells (RBCs) when blood comes in contact with hemodialyzer membrane. It releases hemoglobin in the hemodialyzer [13]. Percentage hemolysis was calculated to determine their suitability for the hemodialysis application. The percentage hemolysis less than 5 is regarded as non-toxic according to ASTM F-756-08 standard. Clearly, the percentage hemolysis values reported are well within the permissible limit which indicated the blood-contact suitability of the prepared HFMs in this study, with PTN-50 HFMs being the best membrane material among all HFMs (Figure 3).

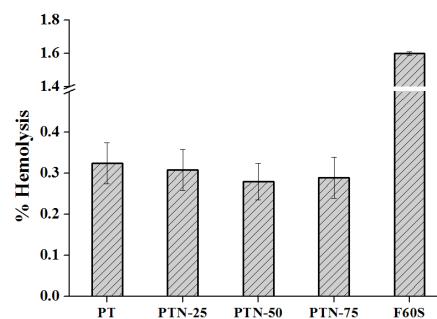


Figure 3: Percentage hemolysis of prepared HFMs. All the membranes are within permissible limits indicating the suitability of membranes for hemodialysis application.

Platelet adhesion: Platelet adhesion and activation are the most crucial events in case of extracorporeal blood circulation [14]. SEM imaging was performed to observe the platelet adhesion and activation morphologically on the inner surface of different HFMs (Figure 4). Less platelet adhesion with no activation was observed in all the prepared HFMs, however, comparatively less platelet adhesion was observed in PTN-50 HFMs indicating the superior suitability for the kidney dialysis.

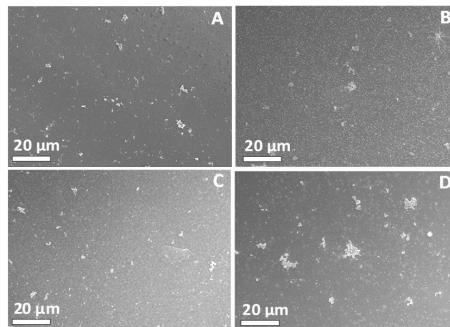


Figure 4: SEM images showing adhered platelets on the inner surface of (A) PT, (B) PTN-25, (C) PTN-50, and (D) PTN-75 HFMs. Least platelets adhesion on PTN-50 HFMs.

3.3 Separation Performance

Ultrafiltration coefficient: K_{UF} determines the flux of a dialyzer, and usually high value of K_{UF} is desirable for kidney dialysis. In this study, with increase in the NZ content in HFMs, the value of K_{UF} increased from 51 mL/m²-hr-mm Hg to 379 mL/m²-hr-mm Hg (Figure 5A). The hydrophilic nature of NZ altered the interfacial polymerization kinetics and membrane structure resulting in enhanced membrane permeability [15].

BSA solute rejection: The efficacy of a membrane material for the hemodialysis application was studied using BSA solute rejection which corroborates to retention of the albumin present in the blood during hemodialysis. Figure 5B shows the comparative performance of all the

membranes tested in the study. % BSA solute rejection for PT, PTN-25 and PTN-50 is comparable to that of the F60S. However, the value is considerably less for PTN-75 which may be attributed to the increased pore size in PTN-75 which resulted in significant loss of BSA. Thus, although the higher value of K_{UF} was achieved with PTN-75 HFM but the low solute rejection may hinder its use for the hemodialysis application. So, PTN-50 HFM was chosen for the uremic toxins removal experiment with goat blood, alongwith PT and F60S HFM.

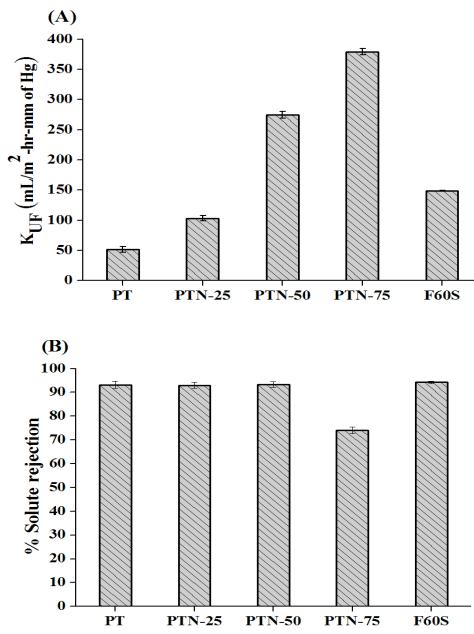


Figure 5: Bar plot showing: (A) ultrafiltration coefficient and (B) BSA solute rejection. The results suggested the safer usability of PTN-50 HFM for the hemodialysis.

Toxin clearance study with toxin-spiked goat blood: The reduction ratio for PT, PTN-50 and F60S HFM is shown in Figure 6. Five-times better uremic toxin separation performance was measured for PTN-50 HFM as compared to that of F60S HFM.

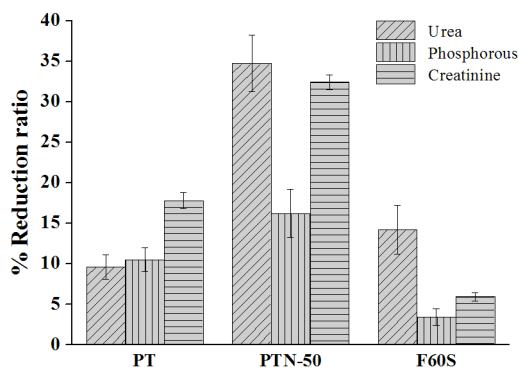


Figure 6: Bar chart showing higher toxin reduction ratio for PTN-50 HFM.

The superior performance of PTN-50 HFM to that of F60S HFM may be corroborated to the following reasons: (1) Vit. E TPGS improved the hemocompatibility, i.e., less hemolysis, low platelet adhesion and minimal activation leading to less side-reactions during hemodialysis. and (2) incorporation of NZ particles improved the porous structures of PT-NZ HFM desired for hemodialysis resulting in increased separation performance.

4 CONCLUSIONS

PTN HFM with high K_{UF} , and improved hemocompatibility were ingeniously fabricated without affecting the BSA rejection and high value of K_{UF} resulting in decreased treatment time. It implies the safer usability of PTN HFM for hemodialysis. The toxin reduction ratio was significantly higher (5-times) for PTN HFM than that for F60S HFM which is due to incorporation of vit. E TPGS to improve the hemocompatibility, and incorporation of NZ particles to improve the porous structures of PT-NZ HFM desired for hemodialysis resulting in increased separation performance. Thus, PT-NZ HFM may be a potential hemodialyzer material for hemodialysis application.

REFERENCES

- [1] Levey AS, Coresh J. Chronic kidney disease. *The Lancet* 2012, 379, 165-180.
- [2] Sinnakirouchen R, Holley JL. Advances in Chronic Kidney Disease 2011, 18, 428-432.
- [3] Saito A, Kawanishi H, Yamashita AC, Mineshima M. *Kidney Blood Press Res* 2012, 35, 299-394.
- [4] Puoci F. Advanced polymers in medicine: Springer 2015.
- [5] Idris A, Yet LK. *Journal of Membrane Science* 2006, 280, 920-927.
- [6] Matsuda M, Sato M, Sakata H, Ogawa T, Yamamoto K-i, Yakushiji T, Fukuda M, Miyasaka T, Sakai K. *Journal of Artificial Organs* 2008, 11, 148-155.
- [7] Idris A, Kee CM, Ahmed I. *Journal Engineering Science Technology* 2008, 3, 172-179.
- [8] Li S, Gao Y, Bai H, Zhang L, Qu P, Bai L. *BioResources* 2011, 6, 1670-1680.
- [9] Idris A, Hew KY, Chan MK. *Jurnal Teknologi* 2012, 51, 67-76.
- [10] Dahe GJ, Teotia RS, Bellare JR. *Journal of Applied Polymer Science* 2012, 124(S1).
- [11] Dahe GJ, Teotia RS, Kadam SS, Bellare JR. *Biomaterials* 2011, 32, 352-365.
- [12] Dahe GJ, Teotia RS, Bellare JR. *Chemical Engineering Journal* 2012, 197, 398-406.
- [13] Peinemann K-V, Nunes SP. John Wiley & Sons 2011.
- [14] Schoorl M, Schoorl M, Nubé MJ, Bartels PC. *Scandinavian Journal of Clinical and Laboratory Investigation* 2011, 71, 240-247.
- [15] Lind ML, Ghosh AK, Jawor A, Huang X, Hou W, Yang Y, and Hoek EMV. *Langmuir* 2009, 25, 10139-10145.