

Design of a noninvasive blood glucose Sensor

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I.P. Brief: MIAO Active Reset and pixel differential amplifier are needed to achieve the pixel Signal-to-Noise at 10^4 .

Keywords: active reset, pixel differential amplifier, Noninvasive glucose monitor, Pulsed Photoacoustic, Monte Carlo simulation, Diabetes, skin optics model.

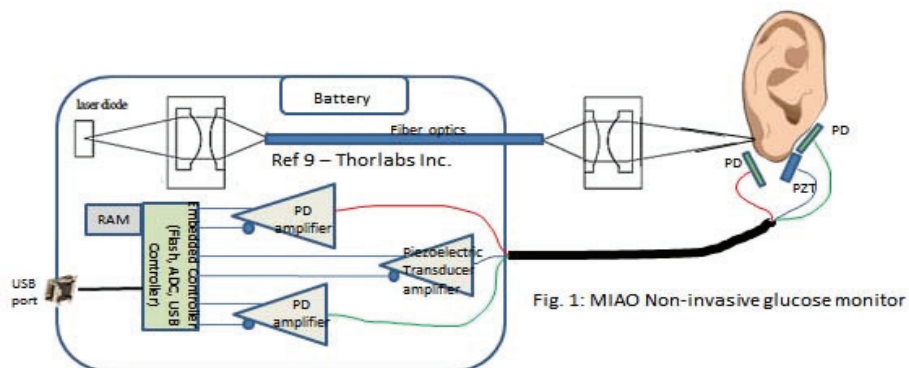
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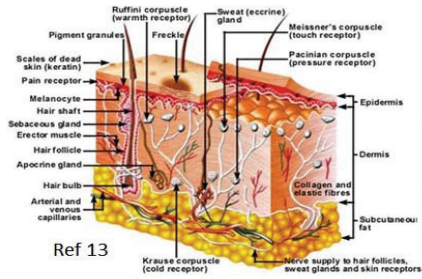
Abstract

This paper describes the design of a non-invasive blood glucose testing device. The Monte Carlo Pulsed Photoacoustic simulation of Figure 1 with the skin optic model in Figure 2 suggests we will need at least a signal to noise ratio (SNR) of 10^4 . This SNR adequate to resolve 1 mili-Mole (mM) glucose variation in a 1 mm path length aqueous solution as wanted by ISO DIS 15197⁵. The needed pixel signal to noise ratio (SNR) is achieved with in pixel differential gain amplifier which provides the pixel conversion gain in mV/e-. The normal CMOS imager typical conversion gain is a few $\mu\text{V}/\text{e}^-$. Further, we substantial reduce the pixel noise to $KT / 100 \text{ Cpd}$ (Figure 5) with MIAO active pixel reset scheme. The prior art of pixel noise are $KT / 30 \text{ Cpd}$ (Pain active reset – Figure 4 Ref 7) and $KT / 18 \text{ Cpd}$ (Fowler active reset – Figure 3 Ref 6). Where Cpd is the pixel diode capacitance, K is Boltzmann constant and T is the temperature.

I. Introduction:

25.8 million Americans (8.3% of the U.S. population) have Diabetes Mellitus with an annual increase rate of 1.3 million cases¹. There is 1.9 million new cases in 2010¹. Diabetes also results in kidney failure, lower limb amputations, blindness, heart disease and stroke⁴. The cost of material used to manage diabetes is roughly \$2,500 a patient for each year. Annual sales of meter and strips are \$1.2 to 1.5 billion in the USA (3 billion worldwide in 2003) and are projected to reached \$10 billion worldwide by 2014^{2,3}. Noninvasive blood glucose recording has been long envisioned to serve as an invaluable tool in prevented or slowed down the debilitating and costly micro-vascular complications of diabetes. The Monte Carlo Pulsed Photoacoustic simulation of Figure 1 with the skin optic model in Figure 2 suggests we will need at least a signal to noise ratio of 10^4 . This SNR adequate to resolve 1 mili-Mole (mM) glucose variation in a 1 mm path length aqueous solution as wanted by ISO DIS 15197⁵.





	$\mu\text{a (mm}^{-1}\text{)}^{10}$	$\mu\text{s}'(\text{mm}^{-1}\text{)}^{10}$	g^{12}	n	$t(\text{mm})^{11}$
epidermis	0.025	0.9	0.9	1.5	0.2
capillaries dermis	0.053	0.93	0.9	1.4	0.2
reticular dermis	0.025	0.9	0.9	1.4	1.5
subcutaneous fat	0.0112	1.08	0.9	1.44	0.3
muscle	0.032	0.59	0.9	1.37	10

Parameters of the skin model

Fig. 2: Skin parameters for Monte Carlo Pulsed Photoacoustic (PA) simulation

II. Low noise and high sensitive pixel design:

The needed pixel signal to noise ratio (SNR) is achieved with in pixel differential gain amplifier which provides the pixel conversion gain in mV/e-. The normal CMOS imager typical conversion gain is a few $\mu\text{V/e-}$. To achieve low read noise and some immunity to common-mode disturbances, a pseudo-differential amplifier with a pinned photo diode (P+/Nwell/Psub) is used. The high conversion gain is implemented with an ADC step size of 100e-. In order to achieve a 10^4 SNR, the readout architecture is Correlated Multiple Sampling (CMS). A summary of current known CMOS imager sampling techniques can be found in Table 1.

Table 1: CMOS imager sampling techniques (Ref.14)

Technique	Offset	Reset	Flicker	Read
Delta-Reset			✓	2x
Correlated Double Sampling	✓	✓		2x
Correlated Triple Sampling	✓		✓	4x
Multiple Correlated Sampling	✓	✓		2x/N
Correlated Multiple Sampling	✓	✓	✓	4x/N

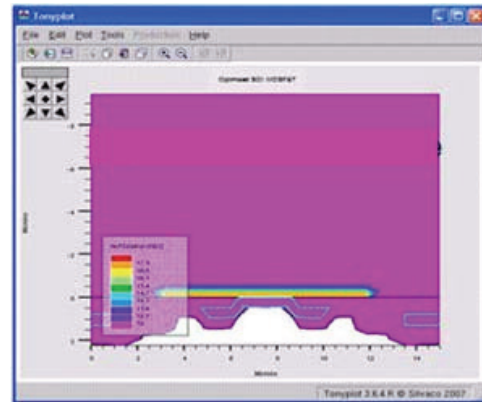


Fig. 7 Optimized pinned photodiode

Cpd (Fowler active reset – Figure 3 Ref 6). Where Cpd is the pixel diode capacitance, K is Boltzmann constant and T is the temperature.

The ATLAS (Silvaco TCAD) simulations of the MIAO pinned photodiode is shown in Figure 7.

The prior art of pixel noise are $KT / 30 \text{ Cpd}$ (Pain active reset – Figure 4 Ref 7) and $KT / 18$

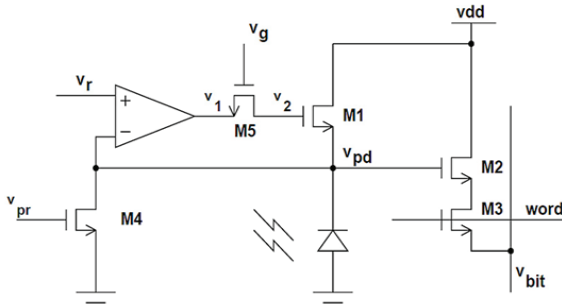


Fig. 3: Fowler active reset (6). Pixel noise $KT/18 \text{ Cpd}$

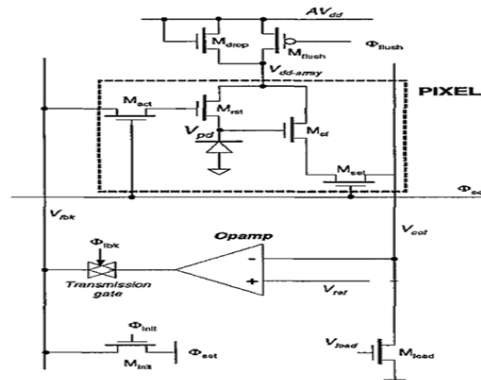


Fig. 4: Pain active reset (7). Pixel noise is $KT / 30 \text{ Cpd}$

Further, we substantial reduce the pixel noise (Figure 5) with MIAO active pixel reset scheme. The innovative active pixel reset is the combination of soft reset (for KT/C noise reduction) with the extended dynamic range (with further lower the noise floor) by clipped pixel based on the barrier stepping concept [18].

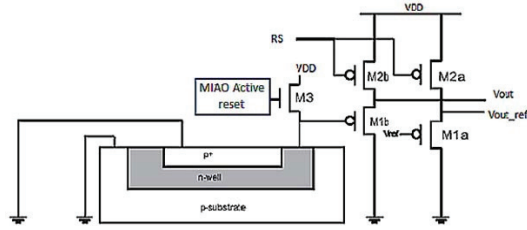


Fig. 5: MIAO active reset. Pixel noise is calculated $KT / 100C_{pd}$

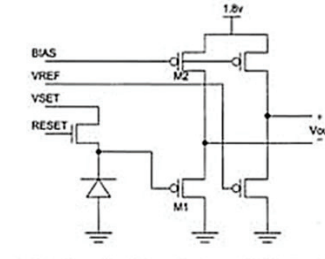


Fig. 6: Pseudo differential amplifier (8)

III. CMOS Image Sensor (PD) Test chip:

The test structure in CRET08 and SPIE08 conference paper [15, 16] is repeated in Figure 8 for clarification purpose.

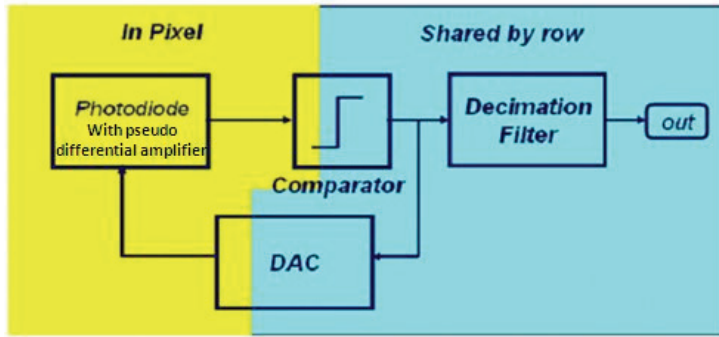
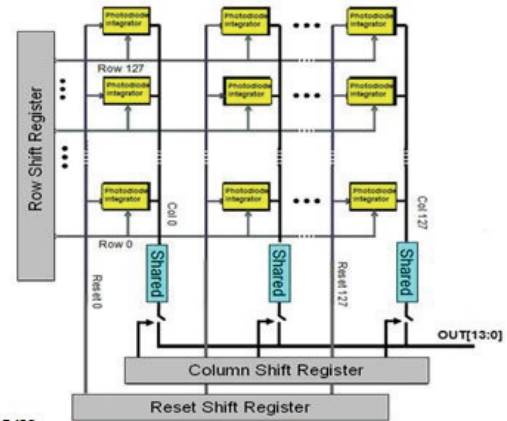


Fig. 9: Simplified Photo Diode sensor test chip block diagram



The Sigma-Delta A/D converter has been chosen because of its ability to reduce DC offset and noise in sampled-data systems. This ability is increased as the sampling rate is increased beyond the Nyquist rate (Over Sampling). Figure 10 is a block diagram of the Sigma-Delta converter [17]. The test chip layout partition is shown in Figure 9.

IV. Piezoelectric sensor

Because of the material's biocompatibility and flexibility, piezoelectric materials have been widely used in applications such as transducers, acoustic components, as well as motion and pressure sensors. In this design, we select the polyvinylidene fluoride (thin-film PVDF) as our piezoelectric sensor due to its unique piezoelectric properties, flexibility, and light weight which is one of the critical requirements for miniature biomedical applications. For the PVDF amplifier, we could use the voltage or charge amplifier configuration. In this project, we select the charge amplifier. The simplify block diagram for the charge amplifier is shown in Figure 11.

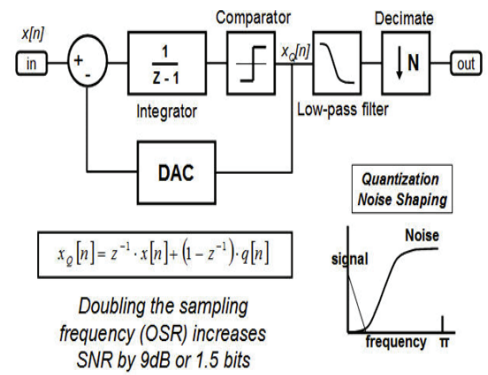


Fig. 10: Sigma-Delta ADC principle

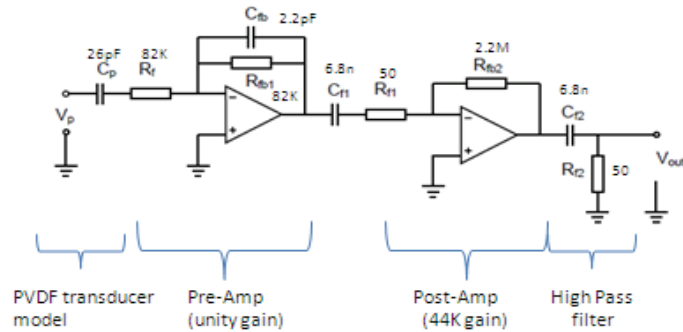


Fig. 11: PVDF Charge amplifier

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